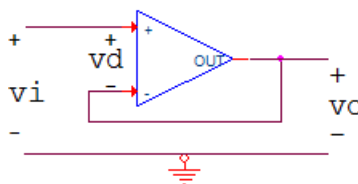


#1. (6 points) For the following circuit

- a) (3 points) Assume that the op-amp is ideal (linear, infinite gain, no input current). Find the transfer function $v_o(s)/v_i(s)$.
- b) (3 points) Next assume that the op-amp gain, v_o/v_d , rather than being infinite, has a first order pole and is given by

$$K(s) = K_o / (s + s_o)$$

where K_o and s_o are real positive constants. In this case find $v_o(s)/v_i(s)$ and give its zeros and poles



#2 (7 points) The standard form for a degree two bandpass filter is

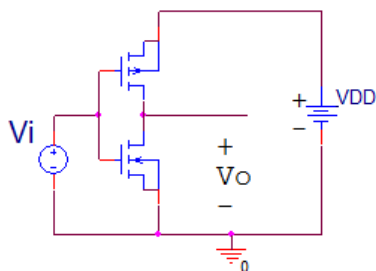
$$T(s, \zeta) = \frac{2\zeta s}{s^2 + 2\zeta s + 1}$$

where ζ is the damping factor .

- a) (4 points) For sinusoidal excitations (that is, when $s=j\omega$) find the peak value of the magnitude $|T(j\omega, \zeta)|$ for fixed ζ .
- b) (3 points) Obtain the sensitivity, S_{ζ}^T , of $T(s, \zeta)$ to the damping factor ζ and give its zeroes and poles. Here the sensitivity of a function f to a parameter x is defined as $S_x^f = \frac{\partial f / \partial x}{f/x}$. (Note: the physical meaning of S_x^f is the relative change of f with respect to the relative change of x).

#3) (7 points) For the circuit below assume that when $V_o = V_i$ both transistors are in saturation with the NMOS described by $I_{Dn} = k_n(V_{GS} - V_{th})^2(1 + \lambda V_{DS})$ and matching PMOS ($|V_{thp}| = V_{th}$; $\lambda_p = \lambda$) except that $k_p \neq k_n$.

- a) (3 points) Show that indeed the two transistors are in saturation when $V_o = V_i$ (recall that saturation means that $V_{GS} - V_{th} < V_{DS}$ for NMOS)
- b) (4 points) For $V_{th} = 1\text{V}$, $\lambda = 0.1$ and $V_{DD} = 9\text{Volts}$, find the ratio k_p/k_n such that $V_i = V_o = 6\text{Volts}$.



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#1. a) By KVL $v_o = v_i - v_d$ but $v_d = 0$ by op-amp virtual input connection
 $\therefore v_o = v_i$ or $\frac{v_o}{v_i} = 1$

b) as above $v_o = v_i - v_d$ but $v_o = K(v_i - v_d) = K(v_i - v_o)$
 $\Rightarrow (1+K)v_o = +Kv_i \Rightarrow \frac{v_o}{v_i} = \frac{+K}{1+K} = \frac{K_0/(1+K_0)}{1+K_0/(1+K_0)} = \frac{K_0}{1+K_0+K_0}$
 $\Rightarrow \frac{v_o}{v_i} = \frac{+K_0}{1+2K_0} \Rightarrow \text{pole @ } 1 = -(1+2K_0)$
 zero @ ∞

#2. We derive ω_m for $|T(j\omega, S)|/d\omega|_{\omega=\omega_m} = 0$ which is $d|T(j\omega, S)|^2/d\omega^2|_{\omega=\omega_m} = 0$

$$a) |T(j\omega, S)|^2 = TT^* = \frac{(25\omega)^2}{(1-\omega^2)^2 + (25\omega)^2} = \frac{(25)^2 \omega^2}{D(\omega^2)}$$

$$d|T(j\omega, S)|^2/d\omega^2 = \frac{(25)^2}{D^2} - \frac{(25)^2 \omega^2 [-2(1-\omega^2) + (25)^2]}{D^3} = 0$$

$$= \frac{(25)^2}{D^2} [(1-\omega^2)^2 + (25)^2 \omega^2 - \omega^2 [-2(1-\omega^2) + (25)^2]] = \frac{(25)^2 (1-\omega^2)^2 [2\omega^2 + 1 - \omega^2]}{D^3}$$

$$= \frac{(25)^2 (1+\omega^2)(1-\omega^2)}{D^2} = 0 \text{ @ } \omega_m^2 = 1 \Rightarrow \omega_m = 1 \text{ (or } -1 \text{ at } |T| \text{ is even in } \omega)$$

(note $D > 0 \forall \omega$)

@ $\omega = \pm 1$, $T(j\omega_m) = \frac{25j \pm 1}{(-1 + 25j(\omega \pm 1))} = \frac{j25}{225} = 1 = \text{max of } |T(j\omega)|$

b) From S^T need $\partial T(\pm j\omega)/\partial S = \frac{25}{\omega^2 + 25\omega + 1} - \frac{25\omega(2\omega)}{(\omega^2 + 25\omega + 1)^2} = \frac{2\omega^3 + 24}{(\omega^2 + 25\omega + 1)^2}$
 $\therefore S^T = \frac{\partial T/\partial S}{T/S} = \frac{S}{25\omega / (\omega^2 + 25\omega + 1)} = \frac{2\omega^3 + 24}{(\omega^2 + 25\omega + 1)^2} = \frac{\omega^2 + 1}{2\omega + 25\omega + 1}$; zero @ $\omega = \pm j1$
 $\text{pole @ } \omega = -5(1 \pm \sqrt{1 - 1/25})$

\therefore the sensitivity is zero at the peak magnitude

#3. a) @ $v_o = v_i$, $v_{DSn} - V_{th} = v_i - V_{th} < v_o$; $-v_{DSp} - (-V_{th}) = -(v_i - V_{th}) > -(v_o - V_{th})$
 \Rightarrow NMOS & PMOS both in saturation
 $\Rightarrow v_i - V_{th} < v_o$ for PMOS

b) Use $i_{Dn} = -i_{Dp}$
 $\Rightarrow k_n (v_i - V_{th})^2 (1 + \lambda v_o) = k_p (+ (v_i - V_{DD}) - V_{th})^2 (1 - \lambda [v_o - V_{DD}])$
 $\Rightarrow \frac{k_p}{k_n} = \frac{(v_i - V_{th})^2 (1 + \lambda v_o)}{(V_{DD} - v_o + V_{th})^2 (1 - \lambda [v_o - V_{DD}])} = \frac{(6-1)^2 (1+0.6)}{(9-6-1)^2 (1+0.3)} = \frac{25 \times 1.6}{4 \times 1.3} = \frac{40}{5.2} = 7.69$
 $= 7.69$